

# **Toward Improved Physics-Based Simulations of the LEO Space Environment using GNSS-Enabled Small Satellites**

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## **Key Points:**

- GNSS-enabled satellites are capable of monitoring the state of the thermosphere at much higher cadences than current operational datasets
- We present an initial technique to infer neutral densities from orbit determination products of the Spire CubeSat constellation
- Densities are used to drive a data-assimilative, physics-based model of the thermosphere and ionosphere during 23 Sept.–9 Dec. 2018

## Abstract

Satellite-atmosphere interactions cause large uncertainties in low-Earth orbit determination and prediction. Thus, knowledge of and the ability to predict the space environment, most notably thermospheric mass density, are essential for operating satellites in this domain. Recent progress has been made toward supplanting the existing empirical, operational methods with physics-based data-assimilative models by accounting for the complex relationship between external drivers and their response in the upper atmosphere. Simultaneously, a new era of CubeSat constellations is set to provide data with which to calibrate our upper-atmosphere models at higher resolution and cadence. With this in mind, we provide an initial method for converting precision orbit determination (POD) solutions from global navigation satellite system (GNSS) enabled CubeSats into timeseries of thermospheric mass density. This information is then fused with a physics-based, data-assimilative technique to provide calibrated global densities.

## 1 Introduction

Within low-Earth orbit (LEO), a region spanning roughly 100 to 1000 km in altitude for the purposes of this paper, interactions between man-made satellites and the ambient atmosphere cause large uncertainties in the orbit determination and prediction processes (Berger et al., 2020). During episodic periods of moderate to severe space weather activity, such atmospheric drag uncertainties can amplify by a factor of 2–5 in a matter of minutes to hours (Krauss et al., 2015; Sutton et al., 2005). These uncertainties, when combined with the steadily growing launch rate of small satellites and CubeSats and our advancing ability to track smaller and smaller objects, are poised to overwhelm the U.S. Department of Defense infrastructure currently carrying out the Detect–Track–Catalog mission. Products of this mission are pervasive across the Space Situational Awareness (SSA) and Space Traffic Management (STM) enterprises and form a critical infrastructure for nearly all space-based activities. Thus, knowledge and prediction of the space environment, particularly the neutral mass density of the thermosphere and lower exosphere, are an essential part of satellite operations within LEO.

One of the major obstacles in predicting orbit trajectories hours to days in advance, and in correlating consecutive or irregular object tracks, comes from the legacy framework used to model the upper atmosphere’s state and its interaction with satellites and debris. The current model employed by the Combined Space Operations Center (CSpOC) and is the High Accuracy

48 Satellite Drag Model (HASDM) (Storz et al., 2005), an empirical model that self-calibrates by  
49 ingesting ground-based tracking data of a select set of orbiting “calibration objects”—i.e.,  
50 operational and defunct satellites passing through LEO with reasonably stable ballistic  
51 coefficients. While this method provides an accurate global-average snapshot of the upper  
52 atmosphere, its abilities to capture realistic spatial structure and forecast into the future are  
53 limited. Physics-based upper atmosphere simulation approaches offer a vast potential  
54 improvement in this regard. Models in this category solve a set of Navier-Stokes fluid equations  
55 that have been appropriately tailored for use in the upper atmosphere and are therefore inherently  
56 better equipped for simulating a dynamic system response to impulsive energy input from the  
57 solar wind. For years the computational cost of these models prohibited their use in an  
58 operational setting. However, present-day computing technology is abundantly capable of  
59 running an ensemble of such models in near real time. Instead, the primary reason that physics-  
60 based methods remain to be adopted by operational centers is the lack of robust data assimilation  
61 schemes capable of self-calibrating at levels equal to or better than those currently used in  
62 combination with empirical models.

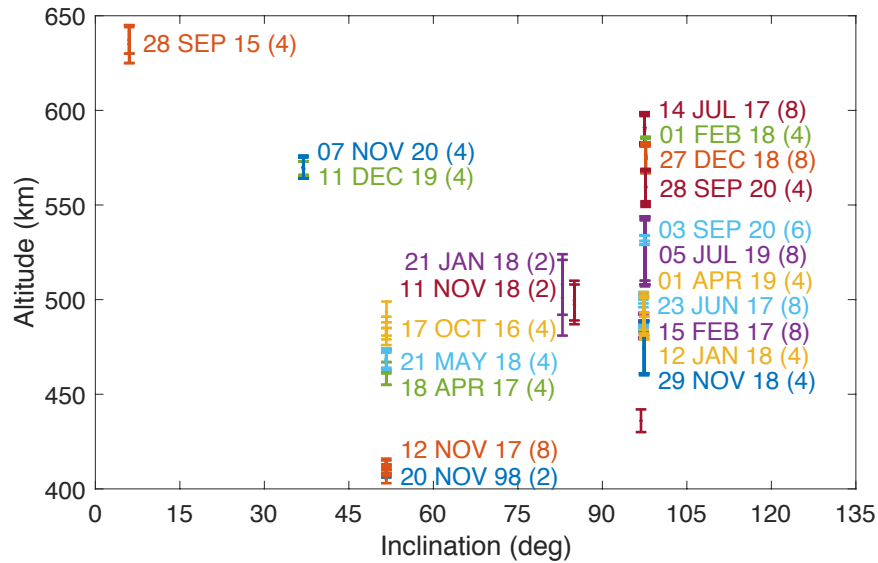
63       Fortunately, significant strides have been made in recent years toward supplanting  
64 empirical methods with physics-based data assimilative models of the upper atmosphere. One  
65 such advancement has been accomplished by accounting for the complex relationship between  
66 external drivers—namely solar flux and geomagnetic heating—and the response of the upper  
67 atmosphere by employing a new least-squares filter called the Iterative Driver Estimation and  
68 Assimilation (IDEA) technique (Sutton, 2018). The new filter operates similarly to an unscented  
69 Kalman filter (UKF) with the addition of mechanisms to accommodate the lagged response of  
70 the upper atmosphere to variations in the external drivers. Using this new technique, notable  
71 improvements in spatial accuracy—even during a geomagnetic storm—have already been  
72 demonstrated (Sutton, 2018), which can help to lower uncertainty across the LEO catalog and  
73 increase the efficiency of Space Traffic Management (STM) activities. In addition, the  
74 emergence of large constellations of commercial and academic CubeSats over the past 5 years  
75 brings with it an excellent opportunity. Most newer SmallSats and CubeSats are equipped with  
76 Global Navigation Satellite System (GNSS) devices, making them valuable sources of Precision  
77 Orbit Determination (POD) information. Many are also equipped with the ability to monitor their

attitude, allowing the construction of an accurate force model. This information can be combined to initialize and constrain models of the upper atmosphere.

In order to track the state of the upper atmosphere with reasonable fidelity, the HASDM model ingests observations from ground-based radar tracks of known objects using a similar technique to the one we present here. However, in order to make strides in specifying and predicting the state of the thermosphere, new data sets with increased resolution, cadence, and coverage are needed (Bruinsma et al., 2021). Satellite-based GNSS observations are capable of describing the space environment at a much higher spatial resolution and temporal cadence. Whereas the conventional radar-derived, satellite-drag data sets operate on a multi-orbit to multi-day cadence, we will show that the GNSS-derived data sets are capable of operating at a cadence of a single orbit. Even higher cadences may also be possible but will require further development. The remainder of the paper details our efforts to use the new set of information provided by CubeSats to drive a physics-based, data-assimilative approach to simulating atmospheric densities in LEO.

## **2 Datasets**

Spire operates a constellation of over 100 CubeSats in LEO with altitudes ranging from 400–650 km and inclinations spanning the globe, from equatorial to polar orbits. Figure 1 gives a snapshot of the distribution of altitude and orbit inclination of Spire CubeSats as of late January 2021.



**Figure 1.** Current coverage of altitude versus inclination for the Spire constellation of CubeSats (as of 26 January 2021). The error bars show the perigee-to-apogee range of altitudes. CubeSats are color coded by common launch dates with the total number of CubeSats in each launch group indicated in parentheses.

The data sets used in this study were provided by Spire Global as part of the NASA Commercial SmallSat Data Pilot Program and cover the period of 23 Sept.–9 Dec. 2018. For the purposes of our work, the following data products were utilized:

- Precision Orbit Determination (POD) solution ephemeris derived from GNSS tracking
- Satellite pointing in the form of attitude quaternions
- Satellite geometry model

POD solutions were typically available during the duty cycle of the GNSS/Radio Occultation (RO) instrument. For the 2018 dataset, duty cycles were in the range of 30–40% of the time, usually concentrated along 40- to 60-minute segments of an orbit (referred to hereafter as an orbit arc). This efficiency has increased with more recent CubeSat builds such that current duty cycles are beginning to approach 100%. For the current data set, ephemeris from each orbit arc were estimated using the RTOrb software ([https://gps-solutions.com/brochures/GPSS\\_Brochure\\_RTOrb\\_Nov\\_2011.pdf](https://gps-solutions.com/brochures/GPSS_Brochure_RTOrb_Nov_2011.pdf)). This software implements a Kalman filter-based approach to estimate orbit ephemeris. As configured for the current dataset, RTOrb considers Earth's gravity up to degree and order 120 from the EIGEN-2 model (Reigber

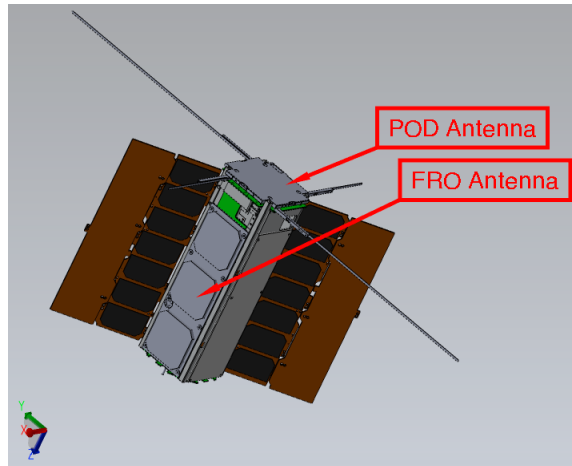
et al., 2003), Luni-Solar 3rd body perturbations, atmospheric drag assuming densities from the Mass Spectrometer Incoherent Scatter extension (MSISE-90) model (Hedin, 1991), and solar radiation pressure (SRP) with cylindrical Earth-shadowing effects. The latter two effects use a cannonball approach in which coefficients of drag and reflectivity are estimated within each arc, respectively, along with the orbit ephemeris. The treatment of drag and SRP in the POD process is not to be confused with the force model described later in this section; instead, the parameters estimated here have little bearing on our calculations of orbit energy.

The attitude of the Spire CubeSats is represented by a quaternion describing the transformation from the body-fixed coordinate system (see Figure 4 below) to the vehicle velocity/local horizontal (VVLH) orbit-based coordinate system at a given instance in time. These data enable the orientation of the satellite with respect to the final coordinate system introduced in Section 3.2. In the initial phases of the NASA Data Pilot assessment, quaternions were provided at an approximate cadence of 10 seconds during the duty cycle of the GNSS/RO receiver, with nothing available outside of the duty cycle. However, it was realized early on in the project that, due to frequent orientation maneuvers, the accuracy of the retrieved neutral densities would be limited by any breaks in continuity of satellite attitude data (see Section 3.3 for further details). The attitude mode of the CubeSats frequently switched between an observing mode aligning GNSS/RO antennas along track and a mode that maximizes the amount of solar flux incident on the solar panels. Because these changes in orientation modify the integrated effect that atmospheric drag has on the orbit parameters, the orientation must be monitored constantly in order to convert orbital energy loss rates to an atmospheric density. Spire has since updated their processing chain for the entire fleet to ensure that a continuous stream of attitude quaternions is available for any datasets originating after 2018. However, for the 2018 data set, processing was limited to a small subset of three CubeSats from Spire Global's constellation for which attitude data had been continuously downlinked and archived. These satellites, which will be used throughout the remainder of the paper, are referred to by Spire's internal satellite ID numbers: 83, 84, and 85. These three CubeSats trace back to a common launch on 21 May 2018 into a  $51.6^\circ$  inclination orbit. During the time period of interest these satellites orbited between the altitudes of 467–492 km. Additional properties and designations of these CubeSats can be found in Table 1.

**Table 1.** Properties of Spire CubeSats used in this study

Spire ID	NORAD ID	COSPAR ID	Perigee/Apogee Altitude (km)	Inclination (degrees)	S/C Mass (g)
83	43560	2018-046G			
84	43559	2018-046F	467–492	51.6	4933 ± 4
85	43558	2018-046E			

Figure 2 shows the geometry for the three Spire CubeSats. The GNSS/POD antenna nominally points in the zenith direction while the front radio occultation (FRO) antenna generally points along the in-track or anti-in-track directions when the satellite is recording RO data. When the RO instrument is cycled off, the satellite reorients in such a way as to maximize illumination of the solar panels.

**Figure 2.** Computer model of Spire's version 3.3 Lemur CubeSat.

### 3 Methods

#### 3.1 Orbital Energy Determination

To drive our data assimilative process, we use information from GNSS measurements taken aboard CubeSats. There are several methods available to infer neutral densities from orbit positioning information. For instance, this can be done by estimating a scaling correction for a density model within a POD solution using two-line element (TLE, e.g., Brandt et al., 2020) sets or GNSS tracking (e.g., van den IJssel & Visser, 2007). We choose instead to employ a model-agnostic energy tracking method that uses the existing POD solutions routinely obtained by

Spire. The first step is to calculate the orbital energy at each available ephemeris data point and track the change in this quantity between subsequent orbits. For an Earth-orbiting satellite, this energy can be approximated in the following way:

$$\xi = \frac{v^2}{2} - \omega_{Earth}^2 \frac{x^2 + y^2}{2} - \frac{\mu}{r} + U_{nonSpherical} \quad (1)$$

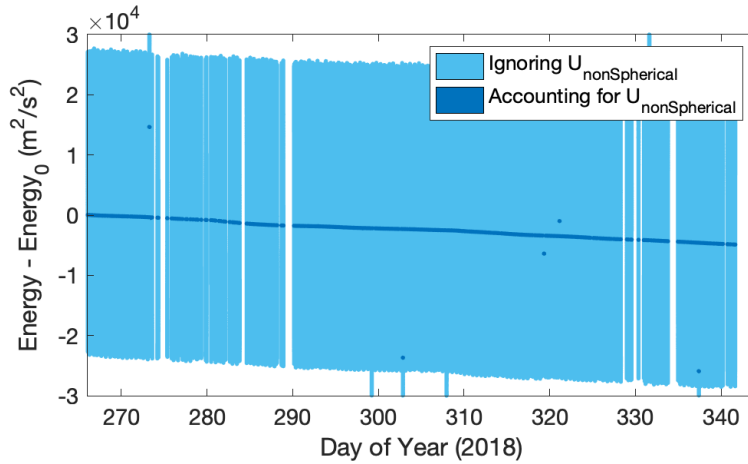
where  $r = \sqrt{x^2 + y^2 + z^2}$  and  $v$  are the satellite's respective position and velocity in an Earth-centered Earth-fixed (ECEF) coordinate frame,  $\omega_{Earth}^2$  is the rotation rate of the Earth,  $\mu$  is the gravitational parameter for the Earth, and  $U_{nonSpherical}$  is a potential function composed of the non-spherical terms of Earth's gravity. In the absence of nonconservative forces (e.g., atmospheric drag or solar radiation pressure) or any additional perturbing conservative forces (e.g., 3rd body attraction, solid Earth tides, ocean tides, atmospheric tides, etc.),  $\xi$  is a conserved quantity along the orbit of a satellite.

We have found that the choice of Earth-fixed coordinates becomes important when considering non-spherical gravity terms in the energy equation (Equation 1), particularly any non-zonal terms (i.e., order  $m > 0$ ). In ECEF coordinates,  $U_{nonSpherical}$  is clearly a function of position alone. The alternate formulation of the energy equation in an inertial coordinate frame, however, would require  $U_{nonSpherical}$  to be a function of both position and time, violating the assumptions underlying a potential function and its use in the energy equation. As a result, the formulation of energy in an inertial coordinate frame does not remain constant along an orbit when considering non-zonal terms—even in the absence of nonconservative forces—and leads to twice-daily oscillations of approximately  $\pm 130$ – $140$  J/kg/s or  $m^2/s^3$  for the orbits analyzed in this paper, or equivalently, about  $\pm 30$ – $35$  m in the semi-major axis. Much of this can be directly attributed to the  $n = m = 2$  gravitational potential term, which is the largest non-zonal term in  $U_{nonSpherical}$ .

If we describe the Earth's gravity field using the two-body approximation—ignoring for a moment the non-spherical contribution—the energy dissipation due to atmospheric drag remains obscured by the large variations in energy due to the J2 and higher-order gravitational terms. The light blue data points in Figure 3 show this simplified calculation of orbital energy for a single CubeSat from Spire Global's constellation (satellite 83) during the period spanning 23 Sept.–9 Dec. 2018. However, when we account for a 36x36 spherical harmonic gravity field as depicted



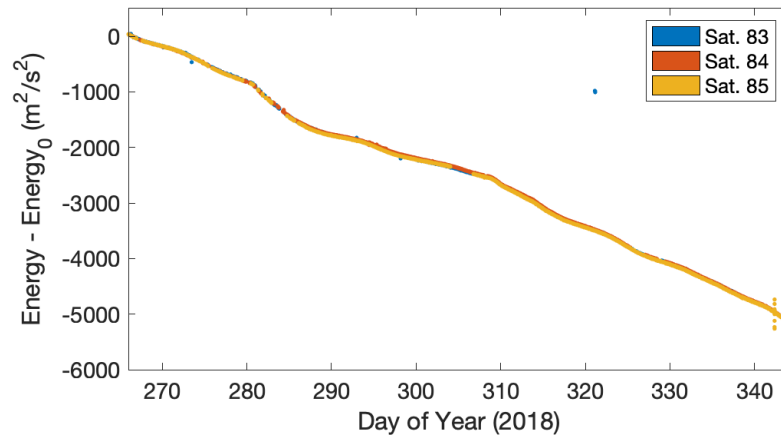
193 by the dark blue curve, the change in energy caused by atmospheric drag is more readily isolated  
 194 from variations in the gravity field.



195

196 **Figure 3.** Keplerian orbital energy (light blue curve, i.e., ignoring the  $U_{nonSpherical}$  term from  
 197 Equation 1) and total orbital energy (dark blue curve, i.e., including the  $U_{nonSpherical}$  term from  
 198 Equation 1) for Spire CubeSat 83 during the period of 23 Sept.–9 Dec. 2018.

199 Figure 4 depicts the orbital energy of all three CubeSats over the same time span as  
 200 Figure 3 but zoomed in to reveal variations in the rate of decay. To conform with the POD  
 201 solutions, we have used the non-spherical terms specified by the EIGEN-2 gravity model  
 202 (Reigber et al., 2003). We found that, for our purposes, including terms above a 36x36 expansion  
 203 yielded diminishing returns.



**Figure 4.** Orbital energy (i.e., including the  $U_{nonSpherical}$  term from Equation 1) for Spire CubeSats 83, 84, and 85 during the period of 23 Sept.–9 Dec. 2018.

During this period of time, the energy curves track one another quite well due, in part, to the fact that all three CubeSats occupy essentially the same orbital plane. Changes in energy were on the order of  $5000 \text{ m}^2/\text{s}^2$  over the entire period of analysis, or about  $65 \text{ m}^2/\text{s}^2$  per day. This is equivalent to a change in the semi-major axis of 1.2 km total, or about 15 meters per day. These magnitudes are specific to the size, shape and ballistic coefficients of the satellites, as well as the altitude and prevailing geophysical conditions sampled during the time period of interest. After applying a simple filter to reject erroneous arcs (note the obvious outliers on day 273, 320, and 342 in Figure 4), the noise level of these timeseries of orbital energy becomes low enough to derive an effective energy dissipation rate between subsequent orbit arcs.

### 3.2 Satellite Force Model

To interpret the timeseries of energy from Figure 4 in terms of the behavior of the upper atmosphere, it is necessary to understand how the satellite drag interaction depends on atmospheric density. The rate at which energy is lost from a satellite's orbit to the atmosphere via the drag force, or the energy dissipation rate (EDR), can be related to atmospheric mass density through the following equation:

$$EDR \equiv -\frac{d\xi}{dt} = \frac{1}{2m} C_D A_{ref} \rho v^3 \quad (2)$$

where  $C_D$  is the satellite's coefficient of drag,  $A_{ref}$  is the cross-sectional area of the satellite projected in the direction of  $v$ , the velocity of the satellite in the ECEF coordinate frame,

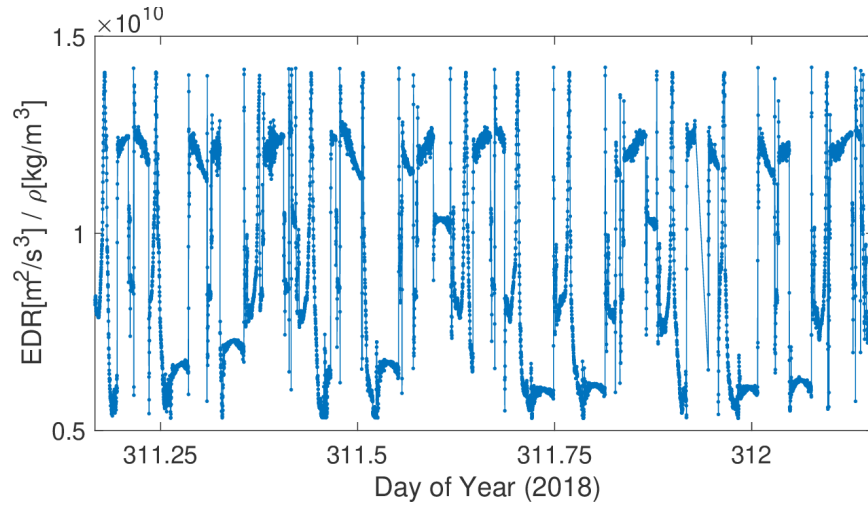
$m$  is the satellite mass,  $\rho$  is the mass density. Winds are neglected in this equation, however, the co-rotation of the atmosphere with the Earth is automatically considered through the use of ECEF coordinates. To compute the coefficient of drag, we consider the transfer of momentum between incoming atmospheric particles and the satellite surface assuming that particles are accommodated to the approximate surface temperature of the satellite using an accommodation coefficient of  $\alpha = 0.93$  (Sutton, 2009). While the accommodation coefficient is kept constant, both  $C_D$  and  $A_{ref}$  can vary significantly over the course of an orbit due to changes in the attitude of the satellite.

In order to compare two subsequent observations of orbital energy  $\xi_0$  and  $\xi_1$  calculated by Equation 1 at their respective epochs  $t_0$  and  $t_1$ , Equation 2 can be integrated to find the dependence on atmospheric density:

$$\xi_1 - \xi_0 = -\frac{1}{2m} \int_{t_0}^{t_1} C_D A_{ref} \rho v^3 dt = -\frac{1}{2m} \rho_{eff} \int_{t_0}^{t_1} C_D A_{ref} v^3 dt \quad (3)$$

Solving for  $\rho_{eff}$ , similar in theme to the work of Picone (2005), gives an effective mass density between  $t_0$  and  $t_1$  along the orbit of the satellite.

Figure 5 shows the simulated change in orbital energy normalized by neutral density ( $EDR/\rho$ ) as given by Equation 2 for one of Spire Global's CubeSats according to its orientation over the course of a single day. This parameter, which we can refer to simply as the force model, is the conversion factor between the observed energy dissipation rate and atmospheric density. The periodic shift between pointing modes—one optimized for RO sensing and the other for solar panel illumination—can be clearly seen in Figure 5. Accounting for the large variations in the force model becomes crucial because a satellite can dwell in a given pointing mode for a significant fraction of an orbit, and this dwell time is not necessarily consistent between orbits. If neglected, these approximate factor-of-two variations in the force model have the potential of causing errors of similar magnitude in the density retrievals.



**Figure 5.** Force model for Spire CubeSat 83 for a single day starting early on 7 Nov. The force model is the conversion factor between the observed energy dissipation rate and atmospheric density.

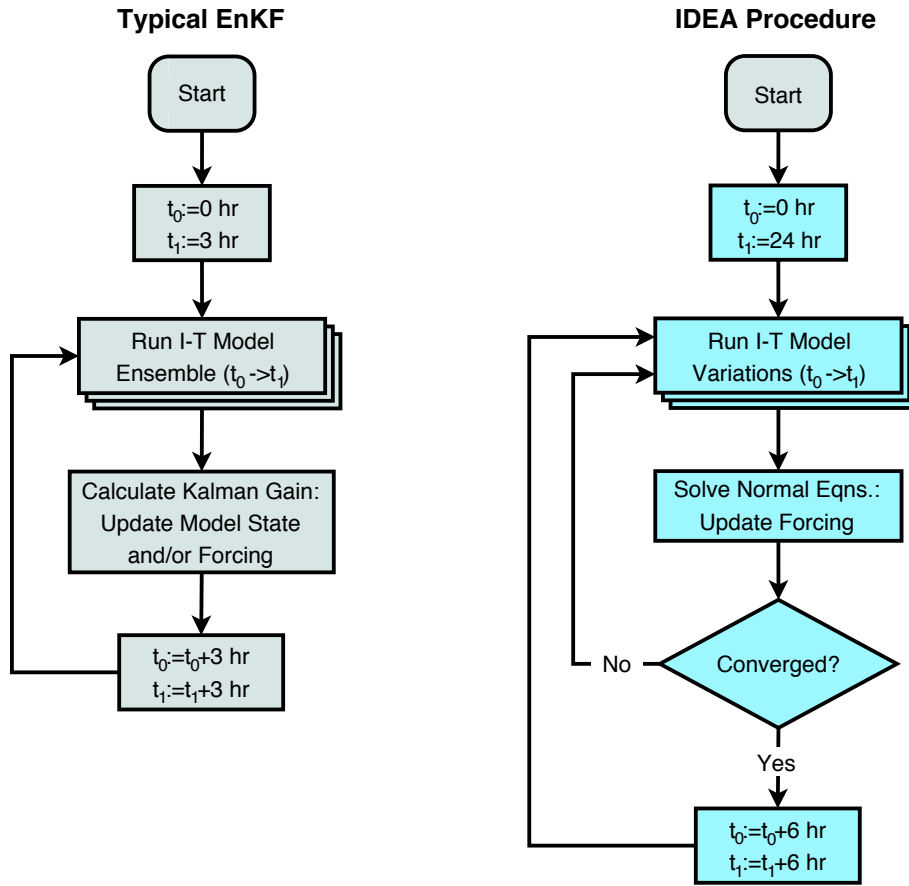
### 3.3 Data Assimilation

After processing the GNSS measurements and applying the force model described above, the final step in our process is to ingest these observations into a data assimilative framework to correct the global upper atmospheric density. Here we briefly describe the Iterative Driver Estimation and Assimilation (IDEA) technique, based on the method of Sutton (2018). This method accounts for the complex relationship between external drivers—namely solar flux and geomagnetic heating—and the resulting response of the upper atmosphere. In general, these drivers are poorly monitored and often rely on proxies that only very approximately represent the physical mechanisms heating and energizing the upper atmosphere. To represent the absorption of solar extreme and far ultraviolet (EUV/FUV) irradiance, the solar radio flux at 10.7 cm wavelength (F10.7) is often used as a proxy. In terms of the solar wind–magnetosphere–ionosphere–thermosphere interaction, the geomagnetic Kp index is often used to characterize heating and momentum exchange at high latitudes. Parameterized coupling functions are then used to convert these proxies into atmospheric heating, incurring further uncertainty into the overall modeling process. The reliance on these proxies and their coupling functions leads to large uncertainties when driving a model of the thermosphere.

IDEA estimates corrections to the external forcing parameters and their coupling functions in order to bring a physics-based model into better agreement with direct observations of the thermosphere. The discrepancies between model output and observations are minimized by employing a least-squares filter similar in nature to an unscented Kalman filter (UKF). Figure 6 compares the IDEA process (right) to that of a typical ensemble Kalman filter (EnKF) configured for ionosphere/thermosphere modeling. IDEA runs several versions of the thermosphere model, each experiencing slightly different external driving conditions.

In the current implementation of IDEA, the Thermosphere–Ionosphere–Electrodynamics General Circulation Model (TIEGCM) (Qian et al., 2014; Richmond et al., 1992; Sutton et al., 2015) is used as the physics-based environment model. TIEGCM is a finite-difference solution to the conservation equations of momentum, mass, and energy describing the upper atmosphere in the presence of momentum and energy sources. TIEGCM accounts for the dominant features in the upper atmosphere of molecular diffusion and circulation, solar heating in the EUV and FUV bands, and high-latitude auroral heating. TIEGCM also has the ability to simulate the ionosphere and associated electrodynamic coupling between the neutral and plasma environment in a self-consistent manner at middle and low latitudes.

In terms of data assimilation, additional measures must be taken to deal with the lagged response of the upper atmosphere to variations in the external drivers. It is well known that the response of the thermosphere can take on a large range of timescales depending on several factors, height being among the largest contributors. In order for an estimated correction of the external forcing parameters to have a timely effect on the model, the time-lagged response must be accounted for. IDEA abandons the sequential filtering techniques typically used for ionosphere/thermosphere applications (e.g., M. V. Codrescu et al., 2004, 2021; S. M. Codrescu et al., 2018; Fuller-Rowell et al., 2004; Godinez et al., 2015; Matsuo et al., 2012, 2013; Minter et al., 2004; Morozov et al., 2013; Murray et al., 2015). Instead, an iterative approach is adopted so that estimated forcing parameters can be re-applied to a simulation over the course of a day so that the model can respond to forcing (refer to the additional feedback loop on the right side of Figure 6).



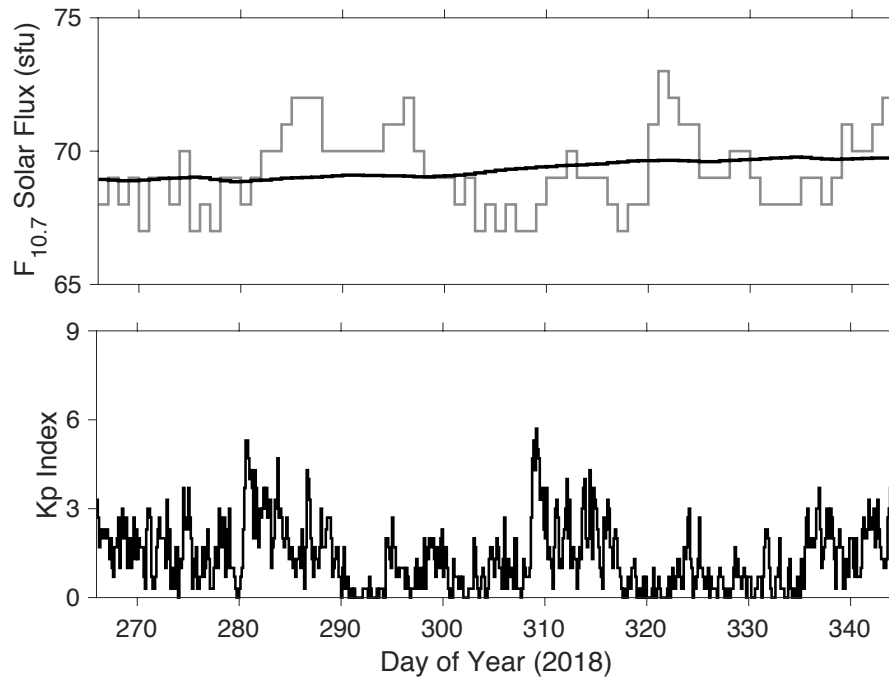
**Figure 6.** Comparison of a typical Ensemble Kalman Filter as configured for use with a time-dependent thermospheric model (left) with the IDEA technique (right; features in color differ from their counterparts in the EnKF flow chart on the left), where  $t_0$  and  $t_1$  are the respective start and end times of the model runs during a given data assimilation cycle (adapted from Sutton, 2018).

In Sutton (2018), satellite-borne accelerometer observations of thermosphere density were used to calibrate the external forcing parameters driving the TIEGCM. Here we use EDRs based on POD ephemeris derived from GNSS measurements from 3 satellites from Spire Global's constellation of CubeSats. A forward model, based on output from the TIEGCM, the satellite geometry model shown in Figure 2, and the force model of Sutton (2009), is used to synthesize orbital energy dissipation for each satellite according to Equation 3. Accelerometer data operates at high cadence (0.1–1 Hz) equating to a resolution of 7–70 km along the satellite's orbit. The GNSS/POD data set yields a measurement of density more on the order of once per orbit arc (possibly higher with additional development). This difference in information content

between data sets necessitates additional consideration when designing a thermospheric estimation filter. In this case, we found that the observability of IDEA was limited to estimation of the most recent daily  $F_{10.7}$  value and the most recent 6-hourly effective Kp value. For comparison, Sutton (2018) found it possible to estimate the most recent daily  $F_{10.7}$  value and the three most recent 3-hourly Kp values when using the high-resolution accelerometer-derived density data set. However, it is expected that improvement in observability will be enabled through the use of more CubeSats in the estimation process. And considering the greater coverage of CubeSats in altitude and local time, accuracy could very easily exceed accelerometer-based density model corrections.

#### 4 Results and Discussion

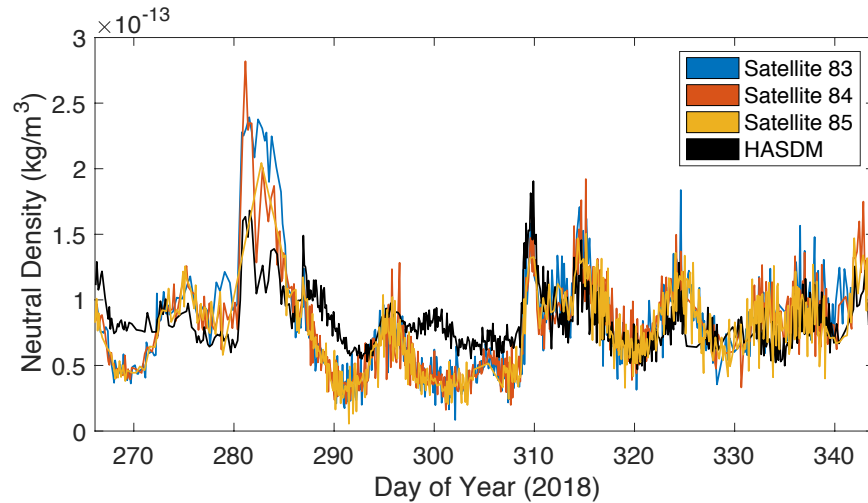
The period spanning 23 Sept.–9 Dec. 2018 (days 266–343) of our study was marked with very low activity in terms of the magnitude and variation of solar EUV and FUV, as approximated by measurements of the 10.7 cm solar radio flux ( $F_{10.7}$ ; top panel of Figure 7). Note that  $F_{10.7}$  has an approximate lower bound of 66 solar flux units (sfu) at solar minimum and attains values above 200 during solar maximum. During the latter, 27-day solar rotational modulation can also produce large swings in  $F_{10.7}$  with concomitant signals in the thermospheric density. Because the 2018 period falls firmly within solar minimum, the variations seen here are quite small. In terms of geomagnetic activity, however, there were two minor-to-moderate disturbances on 7 Oct. (day 280) and 4 Nov. (day 308) as shown by the 3-hourly Kp geomagnetic index (lower panel of Figure 7).



**Figure 7.** Top: observed solar  $F_{10.7}$  radio flux. The grey curve is the daily measured value from the Ottawa observatory normalized to 1 AU sun-earth distance; the black curve is an 81-day ( $\sim 3$  solar rotation) centered average. Bottom: the 3-hourly planetary magnetic index  $K_p$ . Both panels span the period of interest 23 Sept.–9 Dec. 2018.

Given observations of orbital variations and an appropriate force model as discussed in the previous section, an effective atmospheric mass density can be inferred between orbit arcs. Figure 8 shows such neutral mass densities derived from the three CubeSats (blue, red and yellow curves) of Spire’s constellation. The cadence of these densities is approximately one measurement per orbit arc. For the time period studied, this equates to a cadence of about 2–2.5 hours on average. This cadence depends on the instrument duty cycle, which has steadily improved since 2018. A higher cadence may be possible in the future as duty cycle improves, however, the exact allowable cadence will also depend on the altitude of the satellite and the noise errors of the GNSS measurements. HASDM output is also shown with the black curve for reference. This empirical model is calibrated by ground-based radar tracking observations of approximately 70–90 orbiting objects. Because the individual tracking observations are sparse—relative to those available from GNSS—densities derived from this technique have an effective cadence of several hours to several days (Storz et al., 2005).





**Figure 8.** Neutral mass densities derived from Spire CubeSats 83–85. Also shown is output from HASDM as sampled on the orbit of satellite 84. The values plotted are the effective densities (see the right-hand side of Equation 3) between subsequent orbit arcs.

The CubeSat-derived densities maintain good agreement with one another and reasonable agreement with HASDM. As Figure 7 shows, there are several minor to moderate variations in  $K_p$  over the time interval. The signatures of these disturbances are also seen in the neutral densities of Figure 8. There are several deviations between data and model though, most notably around days 270, 290, and 300, where CubeSat-derived densities are significantly lower than HASDM. We have not yet concluded whether model or data are in error during these intervals, since very little ground-truth data exists during this period for validation. Another period of discrepancy exists around the geomagnetic disturbance on day 280, where CubeSat-derived densities experience a much larger storm-time increase. We note that POD data were less frequent during this particular event than during other times. Additionally, attitude data was unavailable for satellite 83 over much of the disturbance, particularly day 282–285. The discrepancy in amplitude during this event could also be a function of the higher cadence of the CubeSat POD data fit spans (5–6 hours during this event) relative to that of the HASDM data fit spans ( $\sim 1$  day or more), in which case, the CubeSat-derived densities would be expected to more accurately resolve the storm-time disturbance.

In general, some noise in the observations and modeled output is expected, with instrumental, data sampling, and geophysical origins. Part of this noise is caused by variations in sampling location for a given data point. In other words, the data points presented in Figure 8 do

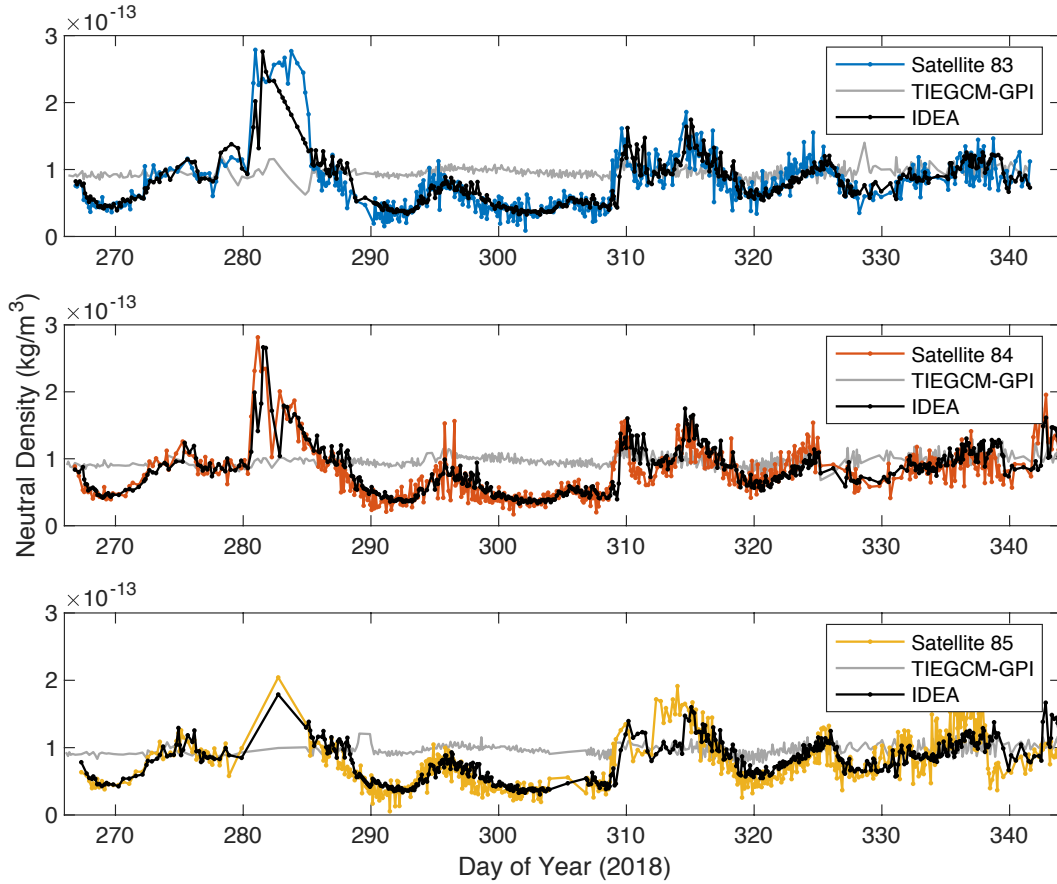
not represent the density averaged over a complete orbit; instead, each data point can be sampled over a very different part of the globe than the previous. The resulting noise can be seen in the HASDM model, which if plotted as an average over full orbits, would appear much more smooth. Another important source of noise in the density timeseries comes directly from uncertainties in the POD solutions themselves. Because the POD solutions were not designed with a thermospheric application in mind, we expect that some of the estimation parameters may have been overfit. And finally, there is certainly an amount of geophysical variability seen in the observed density timeseries that is not captured in by the HASDM model. While an in-depth error analysis is beyond the scope of the present work, we will continue to investigate techniques to minimize this noise, including improving the underlying POD solutions and combining timeseries from additional satellites.

A central goal of this work is to ingest multiple data sources into a physics-based, assimilative thermosphere model to combine information and mitigate the uncertainty of any one dataset. Figure 9 shows the baseline TIEGCM simulation without any assimilation (grey curve) driven externally by the observed geophysical indices (GPI) of  $K_p$  and  $F_{10.7}$ ; the POD-based densities derived using the techniques described in the previous Section (blue, red, and yellow curves); and the IDEA output over the interval spanning 23 Sept.–9 Dec. 2018 (solid black curves).

The baseline TIEGCM-GPI simulation shows muted response to the  $K_p$  and  $F_{10.7}$  inputs during this solar-minimum interval, when compared with the IDEA output (or with the HASDM output in Figure 8). CubeSat densities and IDEA output agree very well over the interval. There are, however, several short periods when POD data from a single satellite becomes sparse, such as the period around day 304–306 for satellite 85 (yellow curve), or when attitude data becomes unavailable, such as the period around day 282–285 for satellite 83 (blue curve). There are also several periods during which data from a single satellite becomes spurious, not agreeing with the data from the other two satellites, such as the period around 335–340 for satellite 85 (yellow curve). In these cases, the other two data sets tend to compensate for missing or spurious data from the third satellite. This leads us to believe that adding data from additional satellites and constellations should improve performance and increase the "signal-to-noise ratio" of the data assimilation process.

The performance of these models with respect to the CubeSat-derived densities are assessed using the metrics of Sutton (2018). These consist of the mean ( $\mu$ ), standard deviation ( $\sigma$ ), and root mean square error ( $RMSe$ ) of the ratio of model density to observed density, all computed in logarithmic space:

$$\mu(m/o) = \exp\left(\frac{1}{N} \sum_{i=1}^N \ln \frac{\rho_{m,i}}{\rho_{o,i}}\right) \quad (4)$$



**Figure 9.** Comparison of observations with model output. CubeSat-derived densities are given by the colored curves for satellites 83 (top), 84 (middle), and 85 (bottom). Also shown is the output from the baseline thermosphere model driven by measured geophysical indices (TIEGCM-GPI, grey curves)  $F_{10.7}$  and  $K_p$ . The data assimilation IDEA output is given along each of the CubeSat orbits by the black curves.

$$\sigma(m/o) = \sqrt{\frac{1}{N} \sum_{i=1}^N \left( \ln \frac{\rho_{m,i}}{\rho_{o,i}} - \ln \mu(m/o) \right)^2} \quad (5)$$

$$RMSe(m/o) = \sqrt{\frac{1}{N} \sum_{i=1}^N \left( \ln \frac{\rho_{m,i}}{\rho_{o,i}} \right)^2} \quad (6)$$

As mentioned in Sutton (2018), these metrics have several properties that are desirable when working with the ratio of a quantity, such as neutral density, that varies exponentially. The  $RMSe(m/o)$  and  $\sigma(m/o)$  quantities are best interpreted as a percentage in the following way:  $\% = 100 \times (\exp \sigma(m/o) - 1)$ . The  $RMSe(m/o)$  is a combination of  $\mu(m/o)$  and  $\sigma(m/o)$ , as can be seen through the following relation:  $RMSe(m/o)^2 = (\ln \mu(m/o))^2 + \sigma(m/o)^2$ . The  $RMSe(m/o)$  is therefore a good indicator of total model errors. However, if the intent is to drive a POD process using the density model, it may be more informative to use the  $\sigma(m/o)$  metric, since a ballistic coefficient is typically estimated per satellite. In practice, this estimated ballistic coefficient will soak up errors not only in the assumed coefficient of drag, but also in the mean bias of the density model. Table 2 shows the overall performance of the three models, TIEGCM-GPI, HASDM, and IDEA at recreating the Spire CubeSat data.

During the period of interest, the IDEA method clearly outperforms HASDM in all three metrics. This is true of both the prior and posterior IDEA estimates of density; the former is a 6-hour persistence forecast of the external drivers while the latter is the fully assimilated solution. It should be noted, however, that IDEA has a clear advantage over the other two models in this comparison, since IDEA assimilates the very data that it is now being validated against. This scenario is somewhat unavoidable, as there is currently a lack of independent validation data sources related to neutral density. Because of this situation, any systematic errors in our data processing or underlying assumptions are not expected to be revealed by this comparison and validation. Instead, our findings are that the IDEA technique, as an estimation filter, has the requisite control authority to sufficiently adjust the model to the assimilated data set.

**Table 2.** Performance metrics of each model with respect to the assimilated Spire Global CubeSat data, calculated over the entire interval spanning days 266–343, 2018.

	TIEGCM-GPI	HASDM	IDEA	
			Prior	Posterior
$\mu(m/o)$	1.37	1.14	1.06	1.06
$\sigma(m/o)$	58.6%	51.7%	38.5%	33.9%
$RMSe(m/o)$	75.1%	55.0%	39.3%	34.7%

## 5 Summary and Conclusions

The increasing crowdedness of the satellite and debris populations in LEO necessitates improvements in how we detect, track, and catalog orbiting objects. Additionally, if we are to avoid catastrophic collisions in LEO, we must also be able to reliably predict the trajectories of satellites multiple days in advance. With the variability of the space environment, particularly thermospheric mass density, being the largest uncertainty in the orbit prediction chain, this study investigates new ways to monitor the upper atmosphere. In this notoriously data-starved region, the instrumentation commonly carried on recently launched LEO SmallSats and CubeSats, particularly GNSS receivers, can provide essential corrections to physics-based models of the thermosphere. Notably, the amount of data available from this new category of observation should continue to scale with the crowdedness of LEO, whereas the current ground-based tracking database remains limited in quantity and resolution.

In the current work, we have applied a post-processing method to the timeseries of POD ephemeris from three CubeSats in Spire’s constellation. This has allowed us to track the time evolution of orbital energy of each CubeSat over an orbit arc. Further application of a satellite-surface force model converts this information into a timeseries of *in situ* atmospheric mass density. By analyzing 78 days’ worth of data from late 2018, we were able to observe the impact of minor and moderate fluctuations in geomagnetic activity during the prevailing solar minimum conditions. We also found good agreement with HASDM, one of the only sources of thermospheric data currently available for comparison. While the resulting timeseries from a single satellite may be prone to errors, identified here simply as a discrepancy between density timeseries derived from co-orbiting CubeSats, this can be mitigated by assimilating timeseries from multiple data sets into a physics-based model of the thermosphere.

Additionally, with more advanced processing methods, it may be possible to lower the noise for timeseries of individual CubeSats. The POD solutions used here were not specifically tailored to the application of measuring density. One potential complication is that overfitting of parameters or insufficient arc size may have led to significant noise in the inferred densities. Future work will focus on improving the POD solutions to reduce noise and finding the optimal size of the POD fitting window as a function of altitude, phase of the solar cycle, satellite geometry characteristics, and GNSS instrument precision and errors. With these improvements in place, it may even be possible to attain higher cadences than a single data point per orbit. This has been demonstrated when using a state-of-the-art geodetic GNSS receiver (van den IJssel & Visser, 2007), but extending this technique to GNSS-equipped constellations would provide much needed global coverage of thermospheric observations. When paired with a suitable assimilative, physics-based models of the thermosphere, there is great potential to lower the uncertainty of orbit predictions across the LEO catalog, improve the accuracy of conjunction assessments, and increase the efficacy of Space Traffic Management (STM) activities.

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